

Optimization of TiO₂-based UV-LED Photocatalytic System for Mixed Dyes and Pharmaceutical Contaminants

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Abstract

To optimize the working efficiency of the novel UV-LED system based on TiO₂ photocatalyst, the influence mechanism of LED lamp arrangement, light source wavelength and working voltage on photocatalytic efficiency was investigated. Acid red 26 (AR 26), acetaminophen (ACT) and diclofenac (DCF) were used as contaminant targets of the photocatalytic system. LED lamp arrangement had almost no effect on the degradation of AR26. However, the degradation efficiency of ACT and DCF was improved under a higher light uniformity. The ACT concentration and DCF concentration at 360 min decreased by 14% and 15%, respectively, with increasing light distribution from 45% to 66.5%. The main reason for this discrepancy in effect was whether the rate-determining step of the degradation mechanism was affected by the light uniformity. The short wavelength and high working voltage of LEDs were conducive to the photocatalytic degradation of contaminants to a different degree. When the wavelength was reduced from 405nm to 365nm, the conversion of AR26, ACT, and DCF increased by 77%, 227%, and 106%, respectively. The conversion rates of AR26, ACT, and DCF increased by 28%, 54%, and 32%, respectively, with voltage increasing from 3 V to 4 V. The data of this work will provide support for optimizing the working efficiency of UV-LED systems based on TiO₂ photocatalysts.

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Keywords: TiO₂ photocatalyst; UV-LED; Lamp arrangement; wavelength; working voltage

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1. Introduction

Wastewater treatment involves all aspects of human life and industrial production. With the rapid development of the printing and dyeing industry, printing and dyeing wastewater is refractory due to its high concentration of pollutants and complex composition, seriously affecting the water environment [1-3]. Azo dyes, which account for 70% of synthetic dyes in wastewater, are carcinogenic and inhibit the growth of aquatic life [4,5]. The azo structure (-N=N-) is one of the key factors that makes

printing and dyeing wastewater difficult to degrade. Besides, pharmaceuticals and personal care products (PPCPs) often exist in water[6]. It has drawn much attention due to the complicated organic compounds involved in PPCPs.

Physical [7,8], biological [9,10], and electrochemical [11,12] methods were proposed to degrade azo dyes and organic compounds. However, biological methods make it difficult to decolorize printing and dyeing wastewater with poor biodegradability. Pharmaceuticals are generally recalcitrant to biochemical process. Adsorption methods require specificity for the adsorbent and the adsorbent lifetime is often short. Electrochemical methods consume too

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much energy, and traditional treatment processes produce a large amount of sludge and require secondary treatment. The photocatalytic oxidation method has attracted widespread attention due to its simple operation, short treatment cycle, and no harmful by-products. This technology employs active free radicals (hydroxyl and oxygen free radicals) to effectively decompose contaminants [13-15]. For the removal of organic compounds from wastewater, TiO₂-based photocatalytic technologies were studied by researchers due to the stable self-regeneration of free radicals via UV light exposure [16,17]. A high-power light-emitting diode (LED) offers the UV source the advantage of high efficiency, stable working power, short start-up time and long life span [18]. However, the temperature of the LED chips would increase dramatically if the heat dissipation was not well operated [19]. Many studies have reported on how to improve the cooling efficiency of LED-UV systems. Chen *et al.* found that an air-cooled radiator and a water-cooled microchannel radiator should be used for the low-power LED chipsets and the high-power LED chipsets, respectively [20]. Seo *et al.* proposed that the cooling performances could be improved by using the ferrofluid as the cooling medium, and the fin heat sink filled with the ferrofluid was also suggested [21]. In general, the liquid as the cooling medium was better than the gas. Our previous work proposed that dyeing wastewater itself was an excellent and low-cost cooling fluid [22]. A novel TiO₂-based photocatalytic system of UV-LED coupling with a wastewater cooler cycle was constructed. the TiO₂/UV-LED photocatalytic system has attracted

increasing attention from the academic community due to its low cost and high energy efficiency, especially in the treatment of pharmaceutical contaminants [23].

Many factors can affect the efficiency of this novel system. All factors that affect the heat dissipation efficiency of LED lights, such as the composition and concentration of wastewater, wastewater flow rate, wastewater temperature, catalyst selection, pH, *etc.*, indirectly lead to different efficiencies of wastewater decomposition. Our previous study found that a low temperature (20 °C) of wastewater improved the long-term operational stability of LED beads, a moderate dose of TiO₂ with strong acid condition (pH=2) further improved the photocatalytic activity. In addition, the effects of the arrangement of LED lights, the range of LED light wavelengths, and system working voltage on the efficiency of the TiO₂/UV-LED photocatalytic system are few reported. Previous research reports often only explored the degradation performance of a single pollutant, either azo dyes or one type of organic compound [24]. Few studies on sewage systems where multiple contaminants coexist were reported. Acid red 26 (AR 26) is a typical fuel dye. Acetaminophen (ACT) and diclofenac (DCF) were typical analgesic drugs and anti-inflammatory drugs in the pharmaceutical industry, respectively.

In this work, the TiO₂-based photocatalytic system of UV-LED is optimized. By studying the impact of the arrangement of LED lights, the LED light wavelengths, and the system working voltage on photocatalytic degradation of multiple contaminants, the optimal working conditions of

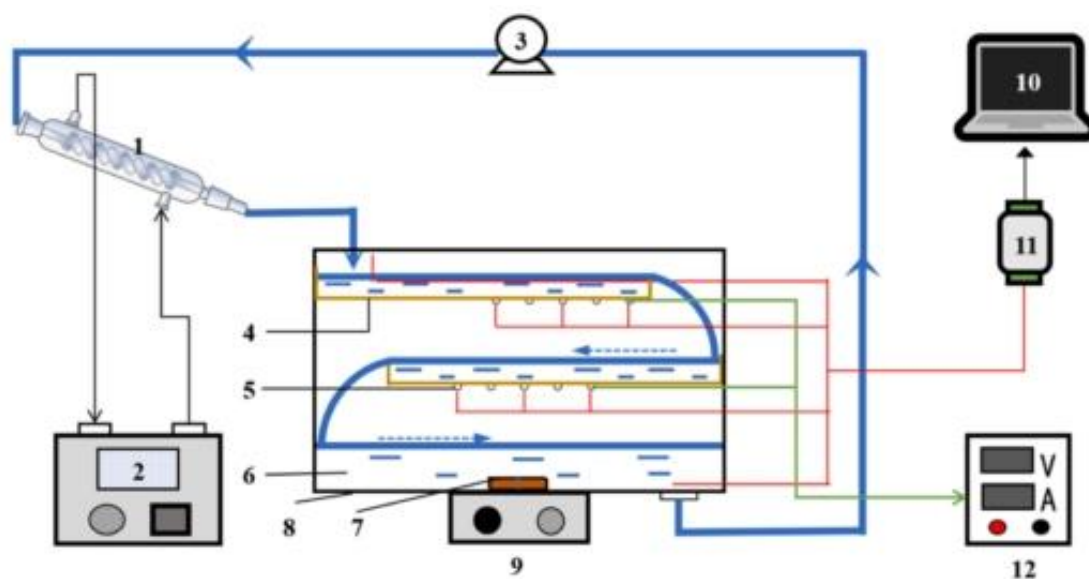


Figure 1. Scheme of the TiO₂-based UV-LED system. (1. Condenser, 2. Thermostatic water bath, 3. Water pump, 4. Copper plate, 5. UV-LED beads, 6. Wastewater, 7. Magnetron, 8. Water storage bath, 9. Magnetic stirrer, 10. Laptop, 11. Temperature sensor, 12. DC power.)

the system were revealed. The degradation of AR 26, ACT and DCF was investigated under different optimized conditions. This work would provide data support for further realizing the engineering application of UV-LED photocatalytic systems.

2. Materials and Methods

The experimental system (Figure 1) is the same as the previously reported [22,25]. The simulated wastewater flows through the heat exchange copper plate of the LED lamp and the sewage tank and circulates at a flow rate of 80 mL/min. AR 26 was bought from Ruji Technology Development Co., ltd China. ACT and DCF were supplied from Sigma-Aldrich, USA. 20 mg/L AR 26, 20 mg/L ACT, 20 mg/L DCF and 0.2 g/L TiO₂ are well dispersed in the 4L deionized water by violently stirred for 40 min. When operating, a constant current DC source (Dazheng, PS-305D 0~30 V/0~5 A) is used as the power supply for UV-LED. The concentration of AR 26 was measured by a UV-Vis spectrometer (Lambda 365, PerkinElmer, Inc., USA) at $\lambda_{\max} = 505.45$ nm. A high-performance liquid chromatography with a UV detector (1260 infinity II, Agilent Technologies, USA) was used to measure ACT and DCF.

The numerical simulation is conducted with the commercial software TracePro. The light intensity distribution under different arrangements of UV-LEDs is calculated. In the model, as shown in Figure 2, the size of the LED substrate is set to 3.45 mm × 3.45 mm. The illumination angle of the LED lamp is set to 120°. The diameter of the upper and lower round table of the reflective bowl is 1.2 mm and 0.65 mm, respectively. The height of the reflector bowl is 0.9 mm. The chip is modeled as a cuboid with the size of 0.4 × 0.4 × 0.15 mm³. The lens of LED is simplified as a thin cylinder with a diameter of 1.2 mm and a thickness of 0.01 mm. The 0.05 lm

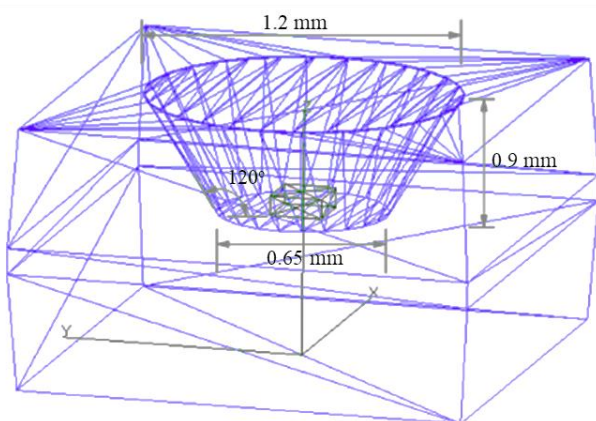


Figure 2. Model of LED lamp bead

luminous flux and 385 nm wavelength are simulated, according to the product manual. 30% of emitted light energy is adopted as 0.345 W for a single lamp. Assume that light passes through the reflective bowl and lens without energy loss. An “ABg” bi-directional transmission distribution function (ABg BTDF) is used as the equation (1),

$$BTDF = \frac{A}{B + |\vec{\beta} - \vec{\beta}_0|g} \quad (1)$$

where, the β and β_0 vectors are from the Harvey-Shack BSDF model. The β vector is the projection of a unit vector in the scattering direction onto the tangent plane, and the β_0 vector is a projection of the unit vector in the specular direction onto the tangent plane. A , B , and g are fitting parameters where A determines the height of the curve, B determines the point where the curve transitions from flat to sloped and g determines the slope.

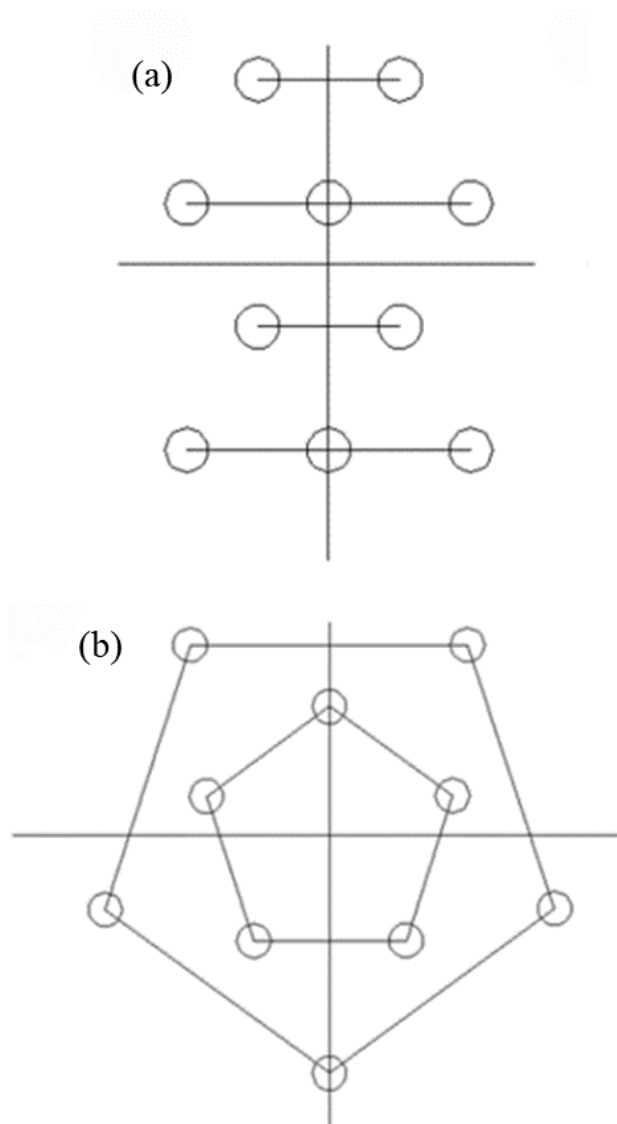


Figure 3. Two arrangement patterns of 10 LED lamp beads: (a) Pattern A and (b) Pattern B

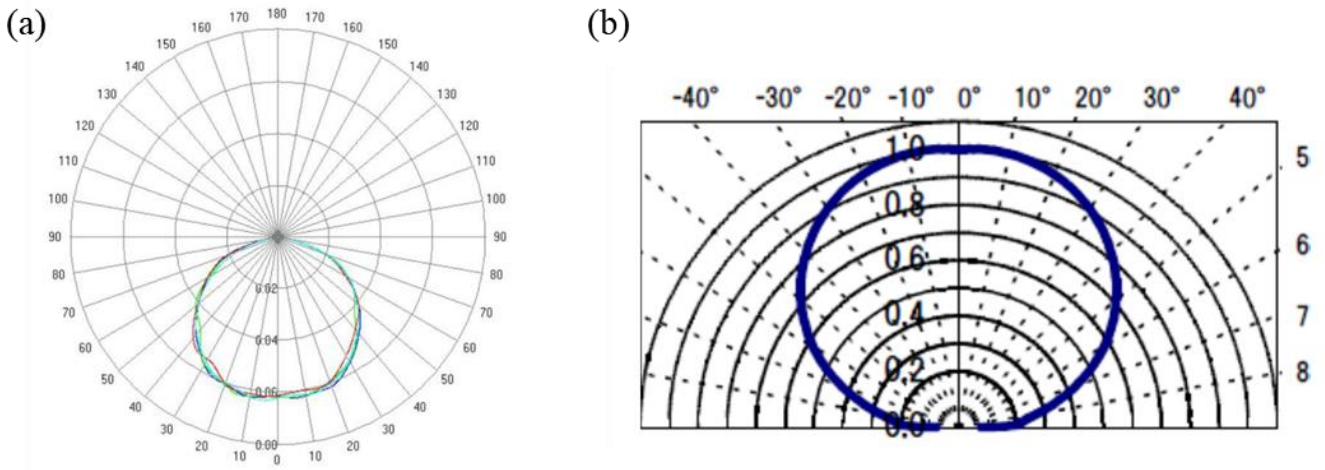


Figure 4. Simulated light distribution curve (a) and real light distribution curve from the manufacturer (b).

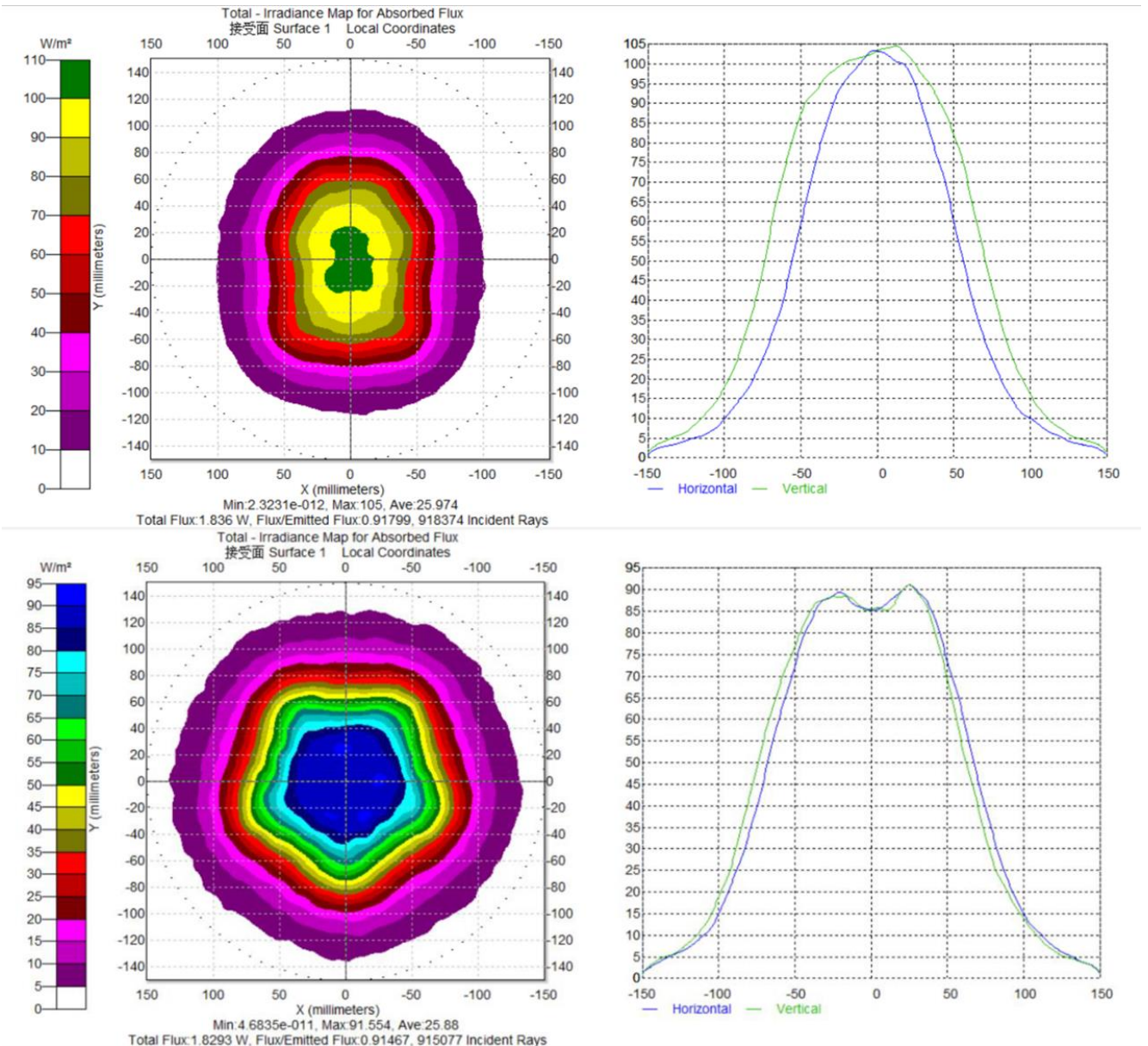


Figure 5. Spatial distribution of light intensity for two LED arrangement patterns.

Generally, A , B , and g are set to 0.35, 0.1, and 0 to model a perfect Lambertian surface. The Monte Carlo algorithm is employed to trace the ray emitted by the LED light source. Considering the calculation accuracy and cost, the total intercepts (traced rays) of ten LEDs for two patterns were set to 100,000 to ensure that the calculation is both efficient and accurate. 100 thousand rays are traced in the calculations for different arrangement patterns. Other reported simulations used similar parameter settings [26].

3. Results and Discussion

3.1 Effect of UV-LED Arrangement

To investigate the effect of LED arrangement on the degradation of wastewater and optimize the LED arrangement, two arrangement patterns of 10 LED lamp beads were examined, as shown in Figure 3. The light intensity was simulated using TracePro simulation software. The light distribution on the wastewater surface (length: 190mm) was calculated by a luminous map. Before calculation, the light distribution curve was validated. The simulated light distribution curve for a single LED lamp is shown in Figure 4(a). Compared to the light distribution curve (Figure 4(b)) offered by the manufacturer, the simulated light distribution curve has the same shape as the real light distribution curve, which shows the effectiveness of the simulation.

As shown in Figure 5, the light intensity emitted by UV-LED arrays for two arrangement

patterns was simulated and analyzed. The luminous flux results on the receiving surface were presented in the form of an irradiation map. The luminous flux on the receiving surface was presented in the form of a ground view. The luminous flux distribution along the horizontal axis section ($Y=0$) and the vertical axis section ($X=0$) is also shown in Figure 5. The results showed that the light intensity of pattern A was more concentrated than that of pattern B. In contrast, the light intensity distribution range of pattern B is wider than that of pattern A. This set of comparison tests controlled the total incident flux and changed the spatial distribution of light.

All the ultraviolet light beams fell within the boundary range (dashed circle). The minimum, maximum, average irradiance and light uniformity can be obtained, as shown in Table 1. Based on the standard of ANSI/NAPM7.228-1997 [27], the irradiation uniformity can be calculated. The average light intensity of the two arrangements was close, which was reasonable due to the same total incident illumination. The light uniformity of pattern A (66.5%) was higher than that of pattern B (45.0%).

To determine the effect of LED arrangement on the degradation rate of AR 26, ACT and DCF, the concentrations of them were detected, as shown in Figure 6. The results showed that the degradation trend of AR 26 has not changed under the two arrangements. However, different LED arrangements had a significant impact on the degradation of ACT and DCF, which degraded

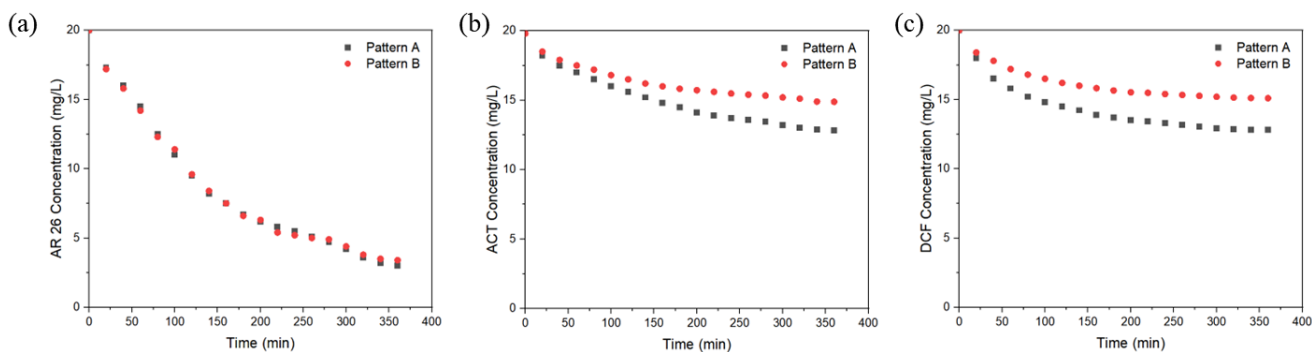


Figure 6. Evolution of concentrations of (a) AR 26, (b) ACT and (c) DCF under two different LED lamp arrangements.

Table 1. Light distribution properties of two different LED arrangements.

| Arrangement | E_{min}^1 (W/m ²) | E_{max}^1 (W/m ²) | $E_{ave}^{2,*}$ (W/m ²) | Light uniformity (%) |
|-------------|---------------------------------|---------------------------------|-------------------------------------|----------------------|
| Pattern A | 2.3×10^{-12} | 105.0 | 25.97 | 66.5 |
| Pattern B | 4.7×10^{-11} | 91.6 | 25.88 | 45.0 |

1. E_{min} , E_{max} and E_{ave} represented the minimum, maximum and average irradiance over the statistical range.

$$2. E_{ave} = \frac{\int_{-0.15}^{0.15} Irradiance(x,y) dx dy}{\pi 0.15^2}$$

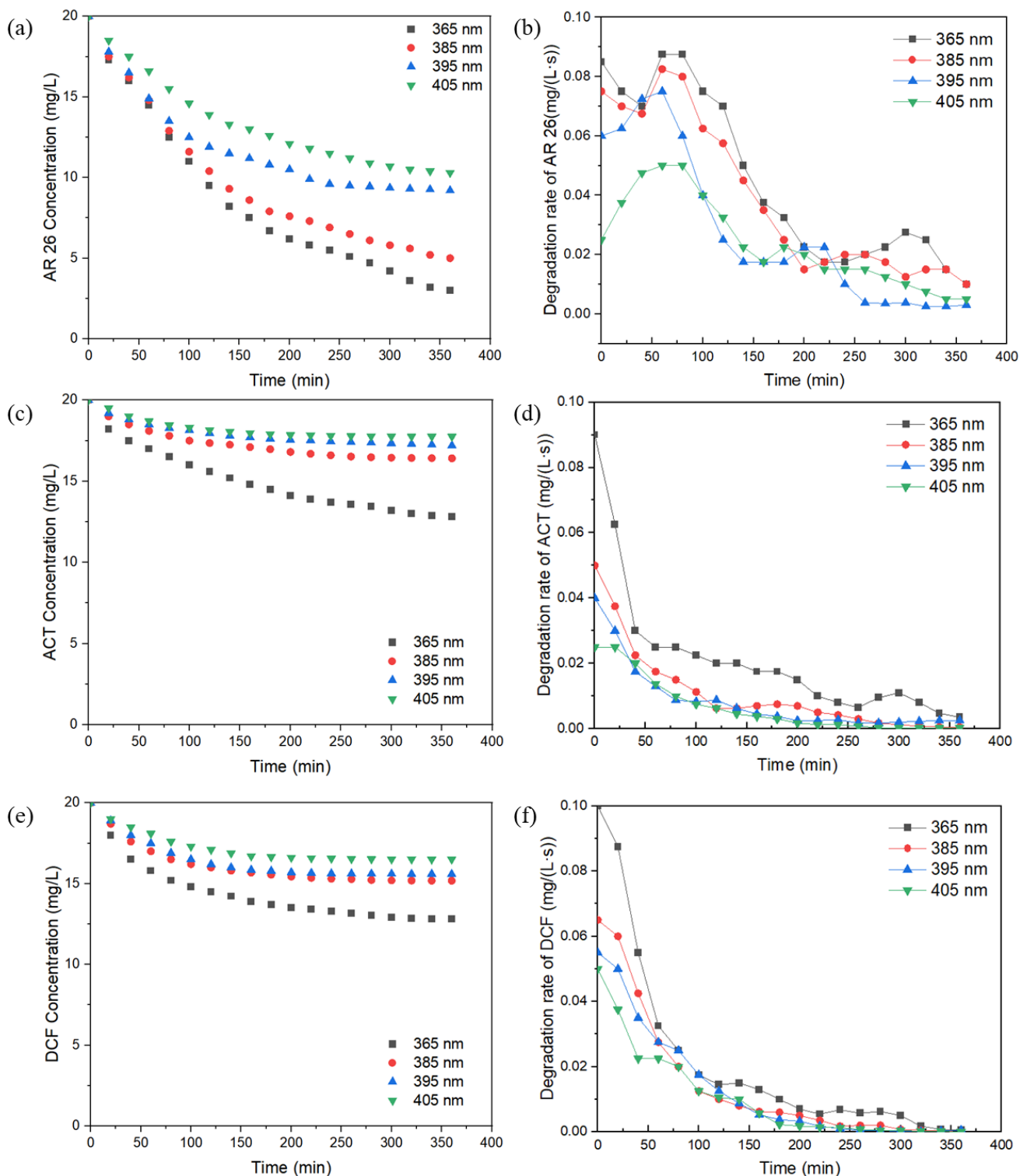


Figure 7. Evolution of the AR 26 concentration and the reaction rate with the different UV LED wavelengths.

Table 2. Specification of UV-LED photoreactor with different wavelengths and the conversion of AR 26 after 360 min reaction.

| Wavelength (nm) | Output power (mW) | Voltage (V) | AR 26 conversion (%) | ACT conversion (%) | DCF conversion (%) |
|-----------------|-------------------|-------------|----------------------|--------------------|--------------------|
| 365 | 300 | 3.2~3.6 | 85 | 36 | 35 |
| 385 | 300 | 3.2~3.6 | 75 | 18 | 24 |
| 395 | 300 | 3.2~3.6 | 54 | 14 | 22 |
| 405 | 300 | 3.2~3.6 | 48 | 11 | 17 |

faster under pattern A of LED lamps. The discrepancy in degradation rates of different contaminants was related to the nature of the contaminants themselves. It can be seen that the degradation rate of AR 26 was much faster than that of ACT and DCF. The degradation of AR 26 was not affected by the LED lamp arrangement, that was the different light uniformity. It indicated that the rate-determining step of the degradation of AR 26 was independent of light uniformity. In contrast, the degradation of ACT and DCF was more difficult, and the rate-controlling step was more affected by light uniformity. The results showed that a higher light uniformity was favored.

3.2 Effect of UV-LED Wavelength

Four wavelengths of Tongjia LED lights (365 nm, 385 nm, 395 nm and 405 nm) were selected to investigate the effect of wavelength on the photocatalytic efficiency. As the reaction progressed, the changes in concentrations of AR 26, ACT and DCF were recorded, as shown in Figure 7. The results showed that shorter wavelength UV-LED was more effective for the degradation of AR 26, ACT and DCF. After 360 minutes of reaction, the conversions of AR 26,

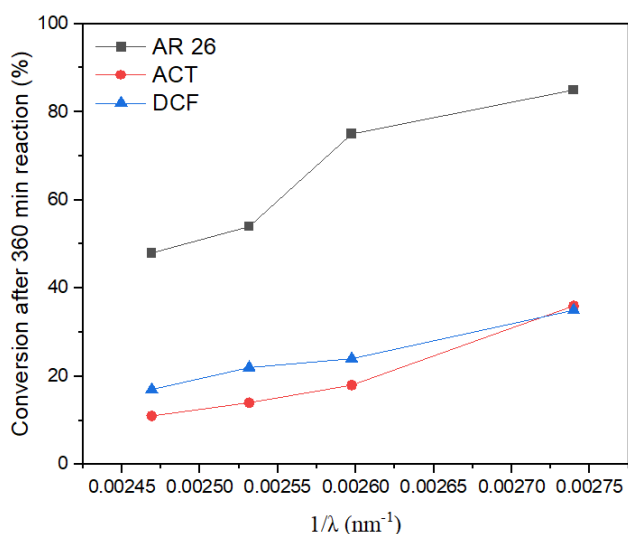


Figure 8. Correlation of degradation efficiency and photon energy (presented as $1/\lambda$) under different wavelengths.

ACT and DCF were shown in Table 2. At a wavelength of 365nm, the conversion rates of ACT and DCF were significantly improved. This might be related to the activation energy of the degradation reactions of ACT and DCF. Note that the wavelength (λ) is inversely proportional to the photon energy (E). The correlation of $1/\lambda$ and the degradation conversion rate after 360 min is shown in Figure 8. It presented that the degradation rates of the three contaminants were basically linearly related to the photon energy. 365 nm or lower number of wavelengths was better employed for improving the photocatalytic efficiency.

Figure 7(b), 7(d), and 7(f) displayed the degradation rate of AR 26, ACT and DCF. The overall degradation rate under different wavelengths gradually decays. Interestingly, the degradation rate increased slightly at 250 min for AR 26 under four wavelengths. The recovery of the degradation rate indicated that the degradation mechanism had changed at this stage. The photocatalytic degradation of AR 26 comprises oxidation, dealkylation, and cleavage of the methoxy group [28]. Each reaction step will produce different intermediates, such as benzene analogs and anthracene analogs. The degradation rate recovery observed in Figure 7(b) required further research due to the complex reaction network. In contrast, no similar changes in degradation rate were observed for ACT and DCF. This was related to their photocatalytic reaction mechanism, normally involving hydroxylation and decarboxylation. The degradation rate of such two pharmaceutical contaminants was very high at the beginning of the reaction, however, the reaction rate decreased fast and the reaction tended to equilibrium.

3.3 Effect of the Voltage

When solar energy is used as a power source to drive UV-LEDs, the intensity of sunlight will alter the driving voltage of the UV-LEDs, which further decides the output power. Three working voltages (3.0 V, 3.5 V and 4.0 V) were investigated. The theoretical output power and wavelength are listed in Table 3. The concentrations of AR 26, ACT and DCF were recorded (Figure 9). The results showed that work voltage significantly

Table 3. Specification of UV-LED photoreactor with different working voltages and the conversion of AR 26 after 360 min reaction.

| Voltage (V) | Output power (mW) | Wavelength (nm) | AR 26 conversion (%) | ACT conversion (%) | DCF conversion (%) |
|-------------|-------------------|-----------------|----------------------|--------------------|--------------------|
| 3.0 | 220 | 365 | 69 | 26 | 31 |
| 3.5 | 300 | 365 | 85 | 36 | 36 |
| 4.0 | 408 | 365 | 88 | 40 | 41 |

affects the degradation of AR 26, compared with ACT and DCF. A higher working voltage facilitated the photocatalytic degradation of AR 26. This was rationalized that a higher working voltage offered a higher output power. In the early stage of the photocatalytic reaction, the instability of the reaction rate similarly occurred. When the reaction was carried out for 250 minutes, the reaction rate also rebounded. This showed that

photocatalytic degradation reactions of AR 26 followed similar reaction kinetics under different light source wavelengths or working voltages. In contrast, the degradation degree and degradation rate of ACT and DCF were not sensitive to the working voltage. The degradation rate was high in the early stage of the reaction but decreased rapidly. After 360 minutes of reaction, the conversions of AR 26, ACT and DCF under

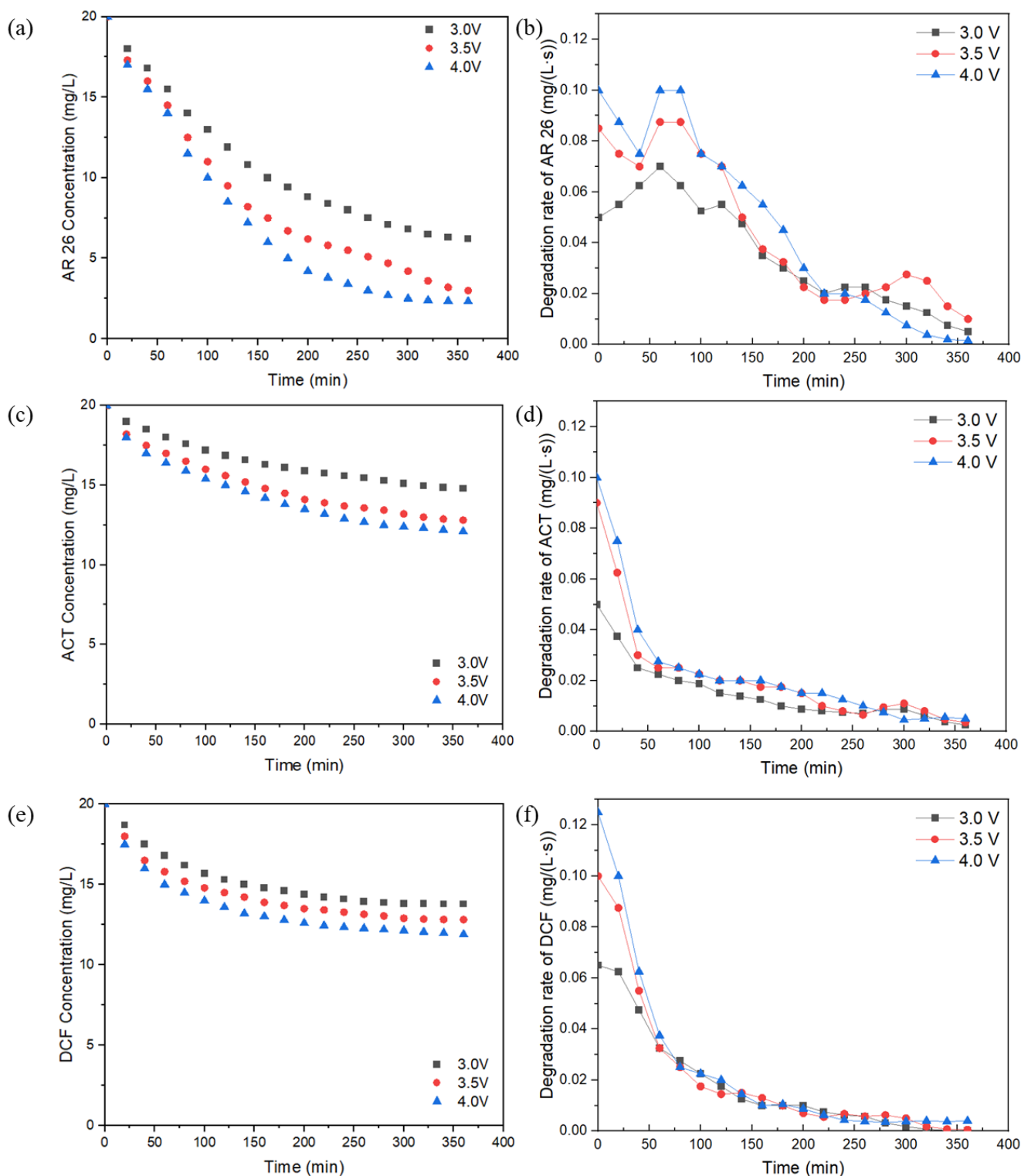


Figure 9. Evolution of the AR 26 concentration and the reaction rate under the different voltages.

different working voltages are shown in Table 3. The correlation of output power with degradation conversion after 360 min was presented in Figure 10. Similar to the results at different wavelengths, the LED output power has a linear relationship with the degradation efficiency. The 4.0 V or a higher working voltage was better employed for improving photocatalytic efficiency.

4. Conclusions

In this work, a homemade photocatalytic test device was set up. The effects of the distribution, wavelength and working voltage of UV LED lamps on the photocatalytic degradation of Acid Red 26, acetaminophen and diclofenac based on TiO₂ catalyst were analyzed. Within the investigated range, higher electrocatalytic efficiency can be achieved on the condition that at 365 nm of LED wavelength, 4.0 V of voltage and 66.5 % of light uniformity. It was found that the output power of the LED light source was a key factor affecting the degradation efficiency of the contaminants. The distribution of LED lights had little impact on the degradation efficiency of AR 26, but had a significant impact on the degradation efficiency of ACT and DCF. This discrepancy was caused by the different rate-determining steps in the degradation reactions for AR 26, ACF and DCF. Wavelengths and working voltages directly determined the output power of LED lamps. Low wavelength and high working voltage improved the photocatalytic degradation rate of AR 26, ACF and DCF. However, different contaminants had different sensitivities to the output power of the LED. This work not only continued the previous optimization of conditions for the AR 26 photocatalytic degradation system, but also used the degradation of two typical

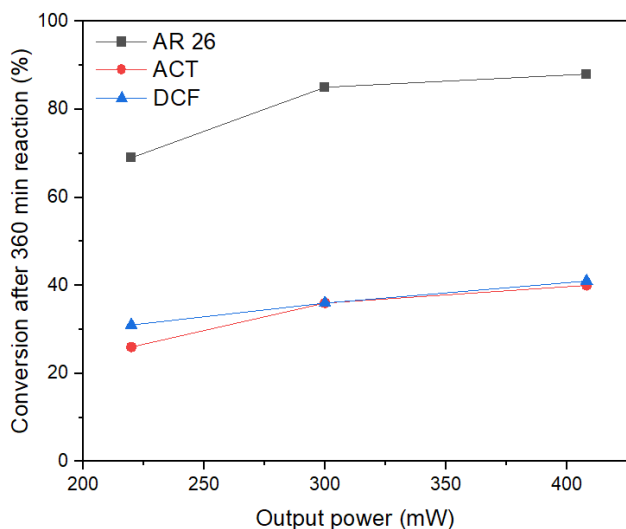


Figure 10. Correlation of degradation efficiency and output power under different working voltages.

pharmaceutical contaminants to verify the system. It helps guide the operating parameters of the TiO₂-based photocatalytic system of UV-LED system application.

CRedit Authors Statement

Zexiang Chen: Conceptualization, Methodology, Investigation, Formal Analysis, Writing Draft Preparation; Chen Wang: Conceptualization, Data Curation, Writing, Visualization, Software; Xue Kang: Validation, Writing, Review and Editing, Data Curation; Yongguo Li: Resources, Review and Editing, Validation, Project Administration. All authors have read and agreed to the published version of the manuscript.

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